



Statistical Model of The Postcombustion Subprocess in an Oven of Multiple Hearth Furnace

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Abstract

Complex multivariable processes are generated in multi-hearth furnaces, and their modeling contains a high index of uncertainty. The main variables that characterize the post-combustion subprocess were identified and data were taken that comprise a period of three months of operation of the installation, to which a regression analysis was carried out step by step backwards. This analysis allowed us to determine that the linear correlation coefficient for hearth temperature four was 0.79 and 0.65 for hearth temperature six, in addition to identifying the independent variables that most influence these process output variables.

Keywords: Furnaces, Post-Combustion subprocess, Regression analysis

Introduction

Nickel-producing companies are characterized by continuous processes of great complexity; that require automation to achieve greater efficiency in their productions. The Company under study operates according to the carbonate-ammoniacal leaching scheme for reduced ore. This company has a multi-hearth reduction furnace plant, which constitutes a key stage in the production process. The reduction furnaces are large metal cylinders, where basically the reduction of nickel oxide and cobalt is carried out to their corresponding metallic forms [1]. In these equipments it is required to maintain a profile of temperature and reducing gases (carbon monoxide and hydrogen), for each hearth, its non-compliance produces significant losses due to the formation of crystalline structures of iron spinels, olivines and pyroxenes that trap nickel and to cobalt in the form of oxides and to a lesser extent in a metallic state, and to the appearance of high contents of metallic iron in the reduced mineral. This results in a decrease in nickel and cobalt extraction in the leaching process [2]. To contribute to the establishment of the thermal profile required by the furnace, secondary air is introduced into hearths four and six (post-combustion), with the purpose of guaranteeing the complete combustion of residual carbon monoxide and other combustible gases that come from incomplete combustion in lower hearths. In this exothermic reaction, an amount of heat is generated that

contributes to the preheating and drying of the mineral. The control loop of hearth four operates automatically and in hearth six manually, as a consequence the chemical physical process that takes place in these hearths is not carried out efficiently; observing temperature oscillations, which affect the thermal and aerodynamic processes that take place in the furnace. The literature consulted shows linear mathematical models for the furnaces of a company with similar characteristics, which operated under different operating conditions [3]. These models were achieved through experimental identification, for mean square fit values between 0.72 and 6.1. Also defined as input variables: the air flow to hearths four and six, and as output variables: the temperature corresponding to these hearths. Montero [4], obtained dynamic mathematical models, with adjustment between 62 and 72%, which characterize the reduction furnaces of the company in question; where they were selected as input variables: the flow of ore fed to the furnace; Air flow to hearths four and six. As output variables: temperature of these hearths and concentration of residual carbon monoxide. To design an effective control strategy for the post-combustion subprocess, it is necessary to know the behavior of the variables in different situations and to obtain a process model. The objective of the work is to obtain a statistical model that represents the behavior of the post-combustion thread.

Materials and Methods

Description of The Reactor

Herreshoff type furnaces [5], are composed of a metal cylinder, in an upright position, lined internally with chamotte bricks or high alumina, protected externally by a metal housing, agitation facilities, feed and discharge of ore and combustion chambers. They are formed internally by 17 hearths or hearths that are shaped like spherical vaults (Figure 1). The furnace has a central rotating shaft to which 68 arms are articulated, four for each hearth. Each arm has, depending on the hearth, eight to 12 vanes or inclined teeth. Depending on the area of the furnace, they will be withholding or sweeping and depending on the odd or even hearths, they will allow the discharge from one hearth to another in the form of zigzag. In peer hearths, the discharge is carried out through 30 holes located equidistant from the periphery, in odd hearths by a hole located in the center around the central axis. The combustion chambers are equipped with high pressure oil burners, which are located two for each hearth in: hearth six, hearth eight, hearth 10, hearth 12; except hearths 14 and 15 that only have one camera. In each chamber: the oil distributor consists of a main valve, a filter to separate impurities, a solenoid valve, a thermometer, a manometer, a flow meter with bypass, a pressure regulator and the burner [6].

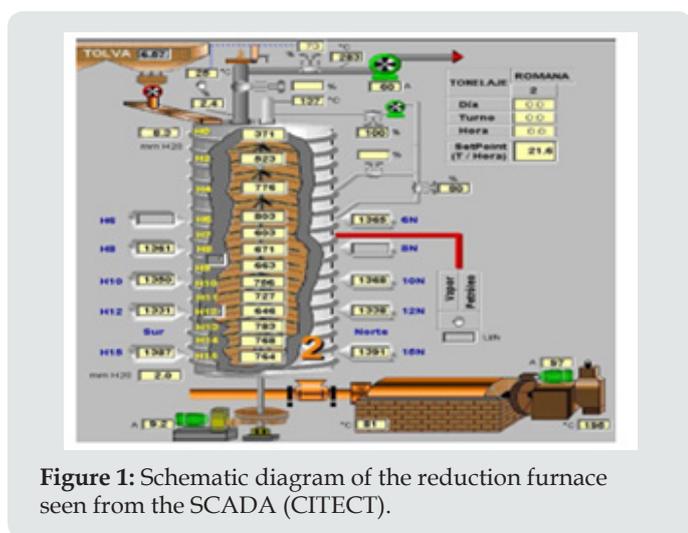


Figure 1: Schematic diagram of the reduction furnace seen from the SCADA (CITECT).

Influence of Temperature in The Reduction Process

Temperature is a fundamental parameter in pyrometallurgical processes, because it facilitates the weakening of the crystalline structures of the mineral and therefore the development of reduction reactions. During the operation, a certain prescribed profile must be maintained, increasing from the top to the bottom, in order to guarantee a gradual heating of the mineral. Special attention is paid to the temperature values of hearths four, 10 and 15. The temperature stability in hearth four is extremely important because of the influence it has on the temperature in the other furnace hearths. If there are temperature values below the norm, there is a displacement of the thermal zones of the furnace, which entails effects on the extraction of nickel and cobalt [7].

Description of The Post-Combustion Installation

The system consists basically of a centrifugal fan (Table 1) installed on the upper floor (ceiling) of the furnace, with hot air suction intake (150 to 200°C) from the chimney from the central axis and an air duct from the fan to hearths four and six, with flow regulation system through butterfly valves. The post-combustion air duct at the fan outlet, it has an internal diameter of 0.407 m and falls parallel to the furnace body to the four hearth, where it branches into two ducts of equal diameter; one goes to hearth four and the other to hearth six (Figure 1). Figure 2 shows the characteristics of the fan for the constant conditions in which it is operating. The fan curve intercepts the system characteristic curve at the operating point (A); for an approximate air flow that circulates before the fork of 6 796 m³/ h, with a pressure of 3 kPa. Considering that the total air flow that is guaranteed before branching is constant and corresponds to a fixed duct air system; are presented in Table 2 airflow hearths four six after the split, according to the valve opening.

Table 1: Technical data of the post-combustion fan.

Fan type	PHD-685 / 100-100S
Rotor speed	233.4 rad / s
Density	855 kg / m ³
Engine	11kW
Fan diameter	685 mm X Size 100%

Table 2: Equivalent air flow based on valve opening.

Opening of the valve	Air flow
to hearths four and six (%)	to hearths four and six (m ³ / h)
10	679.6
20	1 359.2
30	2 038.8
40	2 718.4
50	3 398.0
60	4 077.6
70	4 757.2
80	5 436.8
90	6 616.4
100	6 796.0

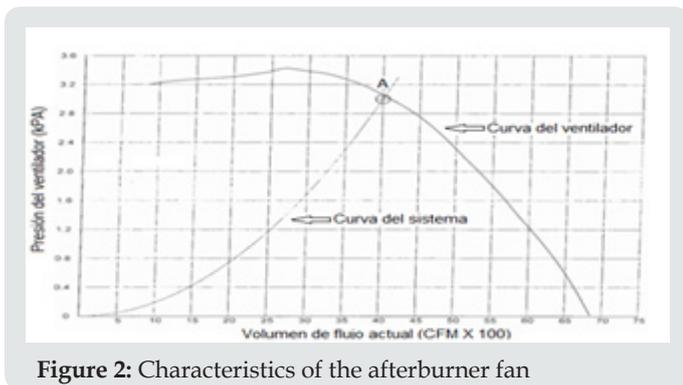


Figure 2: Characteristics of the afterburner fan

Statistical Analysis of The Data

The presentation of the data allows any researcher to easily interpret them. This presentation can be done in two ways:

- a) **Frequency Tables:** It consists of grouping the data into classes or categories with their respective frequencies. It is applicable to any type of variable.
- b) **Graphics:** example (Histogram). It is the representation of the data by rectangles that are based on a horizontal axis and their

area proportional to the frequency of the class interval. They are used primarily for continuous variables.

Regression Analysis

Through a step-by-step regression analysis, the main variables that influence the process-dependent variables are determined, as well as the linear correlation coefficient.

Results and Discussion

As an auxiliary tool to select the variables to be used in the control, a statistical analysis was carried out based on a set of operating data, measured appropriately and continuously. The statistical analysis was carried out with the objective of determining the variables that have the greatest influence on the temperature behavior of hearths four and six of the furnace. For this analysis, five furnace operation data were taken during the months of May to July of a recent year and processed with Microsoft Excel and Statgraphics Plus 5.1 software. These data were obtained from the reports issued by the CITECT Supervisory System. Table 3 shows the average values represented by (X) and the standard deviations by (S) for each of the variables measured in the furnace, which are:

Table 3: Behavior of the furnace variables for three months of work.

Variables	Month					
	May		June		July	
	X	S	X	S	X	S
ApH4	46.2	27.07	35.22	22.6	46.87	22.36
ApH6	24.14	10.91	24.36	10.81	25.68	12.99
TH0	435.92	25.28	424.29	26.2	421.71	24.65
TH2	538.77	35.79	535.318	34.31	528.04	36.11
TH4	718.21	82.33	731.01	76.97	709, 43	77.96
TH6	726.31	62.51	723.51	67.47	702.24	80.32
TH7	557.1	35.25	569.73	40.42	548.37	39.52
TH9	682.73	28.5	673, 22	33.62	658.39	35.77
TH11	725.42	28.72	721.52	37.18	728.61	37.23
TH13	710.53	30.67	705.47	40.35	713.08	33.96
TH14	728.53	37.28	721.14	50.95	735.59	33.73
TH15	764.81	45.81	756.48	68.92	770.39	39.61
PH0	100.85	31.98	74.75	21.48	65.43	28.35
PH16	22.37	24.63	17.27	24.33	17.07	25.02
TC6S	1357.47	118.75	1338.48	170.03	1355.61	118.27
TC8N	1356.82	116.82	1328.4	180.16	1346.16	135.09
TC8S	1348.29	131.98	1328.24	183.11	1352.52	135.96
TC10N	983.54	183.6	1101.14	208.34	1128.98	191 89
TC10S	860.59	57.34	867.01	115.01	839.86	89.27
TC12S	1355.72	110.81	1312.23	232.58	1353.23	115.43
TC12N	1357.21	132.89	1320.75	190.95	1351.29	145.93
TC15S	1358.36	123.31	1280.77	320.61	1350.9	135.13
CO	1.91	1.36	1.04	1.44	1.12	1.44

1. ApH4, ApH6 [Opening of the air flow regulating valve to hearths four and six (%)].
2. TH0, TH2, TH4, TH6, TH7, TH9, TH11, TH13, TH14, TH15 [Hearth temperature zero, two, four, six, seven, nine, 11, 14 and 15 respectively (° C)].
3. PH0, PH16 [Pressure in hearths zero and 16 (Pa)].
4. TC6S, TC8N, TC8S, TC10N, TC10S, TC12N, TC12S, TC15S [Temperature of combustion chambers, hearths six, eight, 12 and 15, north and south side (° C)].
5. CO [Residual carbon monoxide concentration (%)].

In the months indicated above, the post-combustion air flow meter was not installed, so that the openings of the air flow regulating valves to hearths four and six were taken, as proportional measures to the air flow.

The ore processed during this period was of very good characteristics, with a high iron content. A descriptive statistical analysis of the general trend of the thermal profile of hearths four and six during these three months of work, the results of which are presented in Table 4. For this case it is observed that the values of Kurtosis and the Asymmetry Coefficient allow us to state that the dependent variables (temperature of hearths four and six) behave like normal distributions. The frequency histograms for TH4 and TH6 are also presented during the three months of work in Figures 3-8. histogram. With the data for the month of May, a step-by-step regression analysis was carried out to determine the independent variables that most influence TH4 and TH6 (see equations 1 and 2).

$$1) \quad TH4 = -166.9 + 0.3TC8S - 0.5TH0 + 0.13TH13 + 1.4TH2 - 0.8ApH4 - 0.1TH6$$

$$2) \quad TH6 = 171.6 + 0.3TC6S + 0.8TH13 - 1.1TH14 + 0.7TH15 - 0.13TH4 - 0.2ApH4 + 0.6ApH6 + 0.9TH7 - 0.9TH9$$

Table 4: Summary of the descriptive statistical analysis of the sample for three months.

Statistical functions	Month					
	May		June		July	
	TH4	TH6	TH4	TH6	TH4	TH6
Average	718.2	726.3	731	723.5	709.4	702.2
Typical error	0.6	0.4	0.5	0.5	0.5	0.5
Medium	734.9	734.8	748.7	734.7	717.2	710.9
Fashion	498.9	597.9	610.9	607.9	430.9	454.9
Standard deviation	82.3	62.5	76.9	67,5	77.9	80.3
Sample variance	6778.8	3907.9	5923.7	4552.7	6077	6450.9
Kurtosis	2.1	1.4	1.9	2.9	1.9	2.2
Asymmetry coefficient	-1.2	-0.6	-1.1	-1	-0.9	-0.7
Range	593.1	582.1	690.9	624.1	580.7	706.7
Minimum	319.9	473.4	418.3	425.5	352	291.8
Maximum	912.9	1055.5	1109.1	1049.6	932.8	998.5
Confidence level (95.0%)	1.1	0.9	1	0.9	1	1

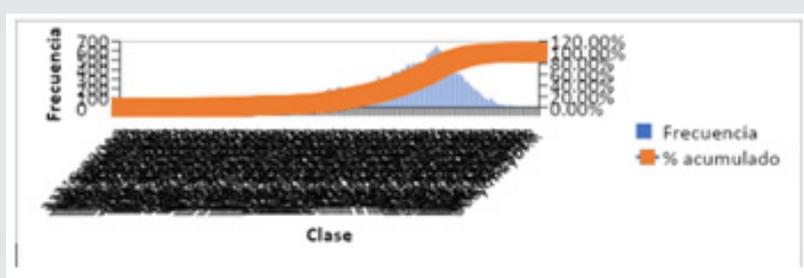


Figure 3: Characteristics of the post-combustion fan

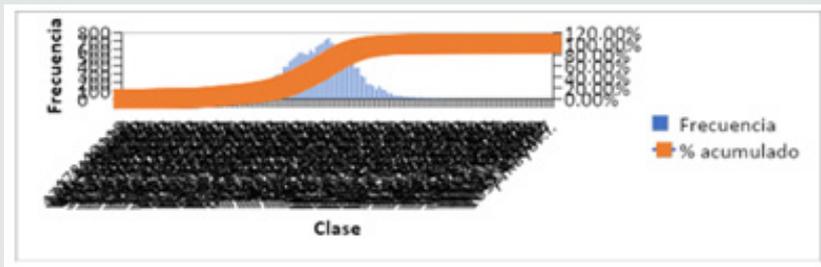


Figure 4: Hearth temperature histogram six (TH6). May

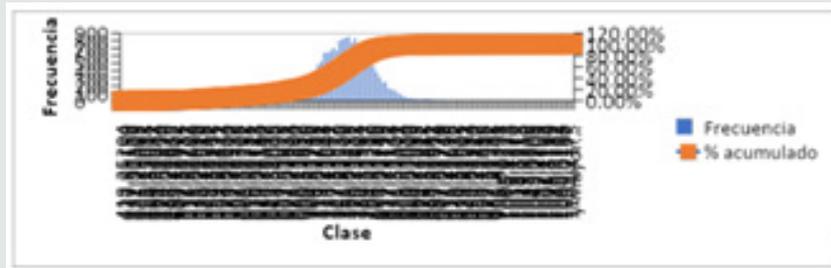


Figure 5: Hearth temperature histogram four (TH4). June

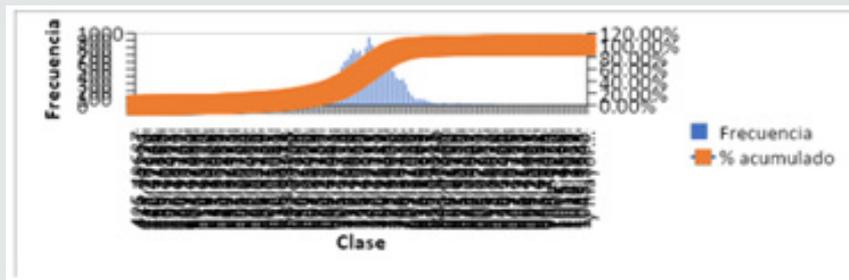


Figure 6: Hearth temperature histogram six (TH6). June

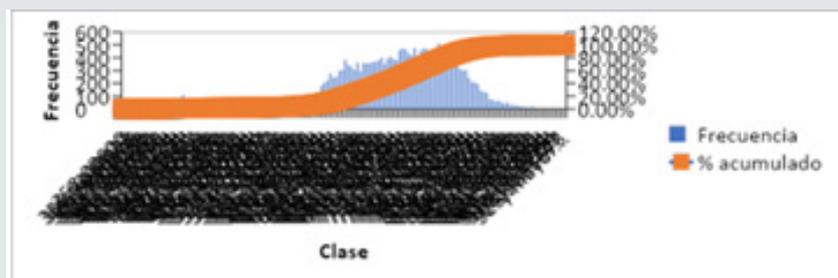


Figure 7: Hearth temperature histogram four (TH4). July

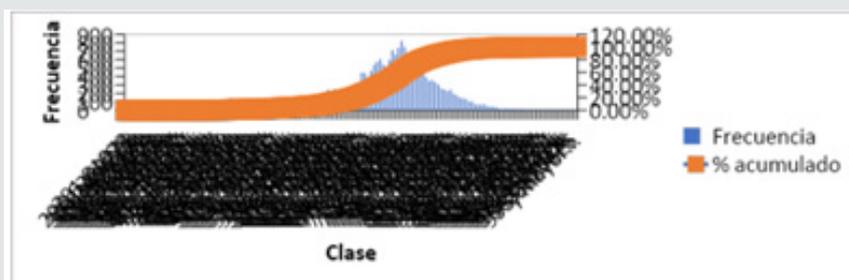


Figure 8: Hearth temperature histogram six (TH6). July

In Table 5, the statistic R^2 indicates that model 1 explains 0.62 of the variability in hearth temperature four, while model 2 explains 0.42 of the variability in hearth temperature six. The statistic R^2 adjusted, which is more convenient for comparing models with different numbers of independent variables, is 0.62 for TH4 and 0.42 for TH6. The standard error of the estimate shows the standard deviation of the residuals, which is 50.62 for TH4 and 47.35 for TH6. Tables 6 & 7 show the analysis of variance for the dependent variables TH4 and TH6. It is noted that the percentages are less than 0.01, so there is a statistically significant relationship between the variables for a 99% confidence level.

Table 5: Summary of the regression analysis for TH4 and TH6.

Regression statistics	Variables	
	TH4	TH6
Multiple correlation coefficient	0.79	0.65
Determination coefficient R^2	0.62	0.42
R^2 adjusted	0.62	0.42
Typical error	50.62	47.35

Table 6: Analysis of variance for hearth temperature four.

Source	Sum of Squares	Degrees of Freedom	Medium Square	Comp. Var.	Percentage
Model	$8,80424 \cdot 10^7$	6	$1,46737 \cdot 10^7$	5 727.11	0.0000
Waste	$5,34722 \cdot 10^7$	20 870	2 562.15	231,765	

Table 7: Analysis of variance for hearth temperature six.

Source	Sum of Squares	Degrees of Freedom	Medium Square	Comp. Var.	Percentage
Model	$3,47949 \cdot 10^7$	9	$3,8661 \cdot 10^6$	1 724.26	0.0000
Waste	$4,67876 \cdot 10^7$	20 867	2 242.18		

Conclusion

As a result of the statistical analysis, the influence of six variables can be seen for hearth temperature four and nine for hearth temperature six. The openings of the air flow regulating valves, which can be manipulated by a final action element, are highlighted. The multivariable nature of the thermal profile of hearths four and six was verified, with respect to the flow of air supplied to these hearths.

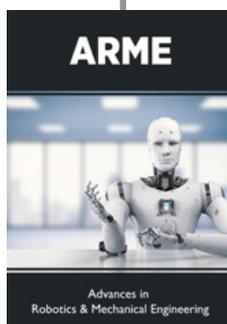
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